## **Vibration Mechanics Hw #3**

## (Harmonically Excited Vibration)

10 Points each. Total 90 Pts.

Issued: Tue. Mar. 19, 2024 Due: Fri. April 12, 2024

## **1.** Rao P. 3.16 Forced response of an undamped system

Equivalent stiffness of wing (beam) at location of engine:

$$k = \frac{\text{force}}{\text{deflection}} = \frac{3 \to I}{\ell^3} = \frac{3 \to \left(\frac{1}{12} \text{ b a}^3\right)}{\ell^3} = \frac{\text{E b a}^3}{4 \ell^3}$$

Magnitude of unbalanced force:  $= m r \omega^2 = m r \left(\frac{2 \pi N}{60}\right)^2 = \frac{m r \pi^2 N^2}{900}$ 

Equivalent mass of wing at location of engine:  $M=\frac{33}{140}~m_w=\frac{33}{140}$  (a b  $\ell$  ho)

Equation of motion:  $M \ddot{x} + k x = m r \omega^2 \sin \omega t$ 

Maximum steady state displacement of wing at location of engine:

$$X = \left| \frac{\text{m r } \omega^2}{\text{k - M } \omega^2} \right| = \left| \frac{\left( \frac{\text{m r } \pi^2 \text{ N}^2}{900} \right)}{\left\{ \frac{\text{E b a}^3}{4 \, \ell^3} - \frac{33}{140} \text{ a b } \ell \, \rho \left( \frac{2 \, \pi \, \text{N}}{60} \right)^2 \right\}} \right|$$
$$= \left| \frac{\text{m r } \ell^3 \, \text{N}^2}{22.7973 \, \text{E b a}^3 - 0.2357 \, \rho \, \text{a b } \ell^4 \, \text{N}^2} \right|$$

## **2.** Rao P. 3.25 Forced response of an undamped system

Equation of motion for rotation about O:

$$\begin{split} J_0 \ \ddot{\theta} = & - k \ \frac{\theta \ \ell}{4} \ \frac{\ell}{4} - k \ \frac{\theta \ 3 \ \ell}{4} \ \frac{3 \ \ell}{4} + M_0 \cos \omega \ t \\ \text{i.e.,} \quad J_0 \ \ddot{\theta} + \left( \frac{5}{8} \ k \ \ell^2 \right) \theta = M_0 \cos \omega \ t \end{split}$$

where  $J_0 = \frac{1}{12} \text{ m } \ell^2 + \text{m} \left(\frac{\ell}{4}\right)^2 = \frac{7}{48} \text{ m } \ell^2 = \frac{7}{48} (10) (1^2) = 1.4583 \text{ kg-m}^2$ 

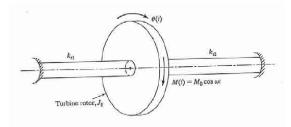
and  $\omega = 1000 \; \mathrm{rpm} = 104.72 \; \mathrm{rad/sec}$ . Steady state solution is:

$$\theta_{\rm p}({\rm t}) = \Theta \cos \omega \, {\rm t}$$

where

$$\Theta = \frac{M_0}{\frac{5}{8} \, k \, \ell^2 - J_0 \, \omega^2} = \frac{100}{5000 \left(\frac{5}{8}\right) \left(1^2\right) - 1.4583 \left(104.72^2\right)} = -0.007772 \, \text{rad}$$

### **3.** Rao P. 3.38 Forced response of a damped system



$$M_t = M_o \cos \omega t$$
,  $K_t = K_{t1} + K_{t2}$ 

Equation of motion:

$$J_0 \ddot{\theta} + c_t \dot{\theta} + (k_{t1} + k_{t2}) \theta = M(t) = M_0 \cos \omega t$$
 (1)

For the given data, Eq. (1) becomes

$$0.05 \ddot{\theta} + 2.5 \dot{\theta} + 7000 \theta = 200 \cos 500t$$
 (2)

steady state response of the turbine rotor can be expressed, similar to Egs. (3.25), (3.28) and (3.29) for a torsional system, as

$$\theta_{p}(t) = \Theta \omega(\omega t - \phi) \tag{3}$$

where

$$\Theta = \frac{M_o}{\left\{ \left( k_t - J_o \, \omega^2 \right)^2 + C_t^2 \, \omega^2 \, \right\}^{\frac{1}{2}}} \tag{4}$$

and

$$\phi = \tan^{-1}\left(\frac{C_{\downarrow}\omega}{\kappa_{+} - J_{o}\omega^{2}}\right) \tag{5}$$

For the given data,

 $J_0 = 0.05$ ,  $M_0 = 200$ ,  $k_t = 7000$ ,  $C_t = 2.5$ ,  $\omega = 500$ Hence Eqs. (4) and (5) give

$$\Theta = \frac{200}{\left[ (7000 - 0.05 \times 25 \times 10^4)^2 + (2.5)^2 (25 \times 10^4) \right]^{\frac{1}{2}}}$$
= 6.2868 × 10<sup>-6</sup> rad

$$\phi = \tan^{-1} \left( \frac{2.5 \times 500}{7000 - 0.05 \times 250000} \right)$$

$$= \tan^{-1} \left( -\frac{1250}{5500} \right) = \tan^{-1} \left( -0.2273 \right)$$

$$= -12.8043^{\circ} = -0.2235 \text{ rad}$$

#### **4.** Rao P. 3.45 Forced response of a damped system

$$\frac{X}{Y} = \left[ \frac{k^2 + c^2 \omega^2}{\left(k - m \omega^2\right)^2 + c^2 \omega^2} \right]^{\frac{1}{2}}.sp$$
or 
$$\frac{10^{-6}}{Y} = \left[ \frac{\left(10^6\right) + \left(10^3 (200 \pi)\right)^2}{\left\{10^6 - \left(\frac{5000}{9.81}\right)(200 \pi)^2\right\}^2 + \left\{\left(10^3\right)(200 \pi)\right\}^2} \right]^{\frac{1}{2}}$$
or 
$$Y = 169.5294 (10^{-6}) m$$

#### **5.** Rao P. 3.47 Forced response of a damped system

m = 100 kg,  $F_0 = 100$  N,  $X_{max} = 0.005$  m at  $\omega = 300$  rpm = 31.416 rad/sec. Equations (3.33) and (3.34) yield:

$$\omega = \omega_n \sqrt{1 - 2 \,\varsigma^2} = \sqrt{\frac{k}{m}} \sqrt{1 - 2 \,\varsigma^2} = 31.416$$
or  $k (1 - 2 \,\varsigma^2) = (100) (31.416^2) = 98,696.5056$ 
For  $k = 0.005$ 

33) and (3.34) yield:  

$$\omega = \omega_n \sqrt{1 - 2 \, \varsigma^2} = \sqrt{\frac{k}{m}} \sqrt{1 - 2 \, \varsigma^2} = 31.416$$
or  $k (1 - 2 \, \varsigma^2) = (100) (31.416^2) = 98,696.5056$ 
and  $X_{max} = \delta_{st} \frac{1}{2 \, \varsigma \sqrt{1 - \varsigma^2}} = \frac{F_0}{k} \frac{1}{2 \, \varsigma \sqrt{1 - \varsigma^2}} = 0.005$ 
or  $k \, \varsigma \sqrt{1 - \varsigma^2} = \frac{F_0}{2 \, (0.005)} = 10,000.0$ 
(2)

Divide Eq. (1) by (2):

$$\frac{1 - 2\,\zeta^2}{\zeta\,\sqrt{1 - \zeta^2}} = 9.8696\tag{3}$$

Squaring Eq. (3) and rearranging leads to:

3) and rearranging leads to:  

$$101.4090 \, \zeta^4 - 101.4090 \, \zeta^2 + 1 = 0$$
 or  $\zeta = 0.0998, 0.9950$ 

Using  $\varsigma = 0.0998$  in Eq. (1), we obtain

$$k = \frac{98696.5056}{1 - 2(0.0998^2)} = 100,702.4994 \text{ N/m}$$

Since  $\zeta = \frac{c}{2 \text{ m } \omega}$ , we find

$$c = 2 \text{ m } \omega_n \ \varsigma = 2 \ (100) \sqrt{\frac{100702.4944}{1000}} \ (0.0998) = 633.4038 \ \text{N-s/m}$$

#### **6.** Rao P. 3.55 Response of a system under the base harmonic motion

$$\ddot{y}(t) = \ddot{z}_{g}(t) = A \cos \omega t \; ; \quad \dot{y}(t) = \frac{A}{\omega} \sin \omega t + B_{1}$$

$$y(t) = -\frac{A}{\omega^{2}} \cos \omega t + B_{1}t + B_{2}$$
Assuming  $y(0) = \dot{y}(0) = 0$ , we get
$$y(t) = -\frac{A}{\omega^{2}} \cos \omega t$$
Equation of motion:

i.e., 
$$m\ddot{z} + k\ddot{z} = -m\ddot{y} = -m\ddot{x}_g(t) = -mA\cos \omega t$$
  
where  $\ddot{z} = x - y$ 

Solution is: 
$$\frac{-mA\cos\omega t}{k-m\omega^2}$$

$$\frac{2(t)}{k-m\omega^2}$$

# : $x(t) = 3(t) + y(t) = -\left(\frac{m}{k - m\omega^2} + \frac{1}{\omega^2}\right) A \cos \omega t$

#### **7.** Rao P. 3.75 Rotating unbalance

Let width = 0.5 m and thickness = t m.

$$I = \frac{1}{12} (0.5) t^3 = \frac{t^3}{24} m^4$$

$$K = \frac{3EI}{I^3} = \frac{3(2.07 \times 10^{11})(t^3/24)}{(5)^3} = 2.07 \times 10^8 t^3 N/m$$

$$\Theta_{11} = \sqrt{\frac{K}{M + 0.2357 m}}$$
Where  $m = \text{mass of beam} = (5 \times 0.5 \times t)(\frac{76.5 \times 10^3}{9.81}) = 19495.41t$ 

$$K_{12} = \sqrt{\frac{2.07 \times 10^8}{75 + 0.2357(19495.41t)}}$$

$$V = \frac{\omega_{11}}{\omega_{11}} = \frac{125.664}{110} \sqrt{\frac{75 + 4595.0688 t}{2.07 \times 10^8 t^3}}$$

$$V = \frac{5st}{|\Gamma^2 - 1|} = \frac{5000}{|\Gamma^2 - 1|}$$
i.e., 
$$0.5 = \frac{5000}{(2.07 \times 10^8 t^3) \left\{ (125.664)^2 \left[ \frac{75 + 4595.0688 t}{2.07 \times 10^8 t^3} \right] - 1 \right\}}$$
i.e., 
$$1.3108 \times 10^4 t^3 - 4595.069 t - 74.367 = 0$$
By trial and error, the value of t is found as
$$t \approx 0.6 m$$
Since this is too large, we can start with a new width such as

**8.** Rao P. 3.92 Coulomb damping

m = 25 kg, k = 10000 N/m, 
$$\mu = 0.3$$
  
 $\omega = 8$  Hz = 50.2656 rad/s  
 $X = 0.2$  m  
Eq. (3.88) gives  
 $C_{eg} = \frac{4 \mu N}{\pi \omega n} = \frac{4 (0.3) (25 \times 9.81)}{\pi (50.2656) (0.2)}$   
= 9.3183 N-8/m

Note: It is assumed that friction force is small compared to Fo in finding the equivalent viscous damping constant of the system.

# **9.** Rao P. 3.97 Other types of damping

Damping force =  $F = C(\dot{x})^n$ Energy dissipated per quarter cycle during harmonic motion  $x(t) = X \sin \omega t$ is  $\frac{\Delta W}{4} = \int_{0}^{\pi/2\omega} c(\dot{x})^n dx = \int_{0}^{\pi/2\omega} c(\omega X \cos \omega t)^n dx$ But  $dx = \dot{x} dt = \omega X \cos \omega t dt$ 

$$\Delta W = 4c \omega^{n+1} X^{n+1} \int_{0}^{\pi/2\omega} \cos^{n+1} \omega t \, dt$$

$$= 4c \omega^{n+1} X^{n+1} \left\{ \frac{1}{(n+1)\omega} \cos^{n} \omega t \cdot \sin \omega t \middle|_{0}^{\pi/2\omega} + \frac{n}{n+1} \int_{0}^{\infty} \cos^{n-1} \omega t \, dt \right\}$$

$$= 4c \omega^{n+1} X^{n+1} \left( \frac{n}{n+1} \right) \int_{0}^{\pi/2\omega} \cos^{n-1} \omega t \, dt$$

Equating this expression to T Ceq w x2, we obtain

$$c_{eg} = \frac{4c \omega^{n} X^{n-1}}{\pi} \left(\frac{n}{n+1}\right) \int_{0}^{\pi/2\omega} \cos^{n-1} \omega t dt \equiv c \omega^{n} X^{n-1} \alpha'_{n}$$
where 
$$\alpha_{n} = \frac{4}{\pi} \left(\frac{n}{n+1}\right) \int_{0}^{\pi/2\omega} \cos^{n-1} \omega t dt = --- (E_{1})$$

For example, for n=2, (E1) becomes

$$\alpha_n = \frac{4}{\pi} \left(\frac{2}{3}\right) \int_0^{\pi/2\omega} \cos \omega t \cdot dt = \frac{8}{3\pi} \left(\frac{\sin \omega t}{\omega}\right)_0^{\pi/2\omega} = \frac{8}{3\pi\omega}$$
and hence  $C_{eg} = \frac{8c \omega X}{3\pi}$ 

which can be seen to be same as the expression found in Example 3.7.

For few other values of n, on can be found as follows:

The amplitude can be found as

$$X = \frac{F_0}{\sqrt{(k - m \omega^2)^2 + c_{eq}^2 \omega^2}} = \frac{F_0}{\sqrt{\kappa^2 (1 - r^2)^2 + c_{eq}^2 \omega^2}}$$

$$= \frac{F_0}{\sqrt{\kappa^2 (1 - r^2)^2 + c_0^2 \omega^2 (n+1)}} X^{2(n-1)} \times \frac{\pi^2}{\kappa^2}$$