Vibration Mechanics Hw #3

(Harmonically Excited Vibration)

10 Points each. Total 90 Pts. Issued: Tue. Mar. 19, 2024

Due: Fri. April 12, 2024

1. Rao P. 3.16 Forced response of an undamped system

Equivalent stiffness of wing (beam) at location of engine:

$$
k = \frac{\text{force}}{\text{deflection}} = \frac{3 \text{ E I}}{\ell^3} = \frac{3 \text{ E } \left(\frac{1}{12} \text{ b a}^3\right)}{\ell^3} = \frac{\text{E b a}^3}{4 \ell^3}
$$

Magnitude of unbalanced force:
$$
= m \text{ r } \omega^2 = m \text{ r } \left(\frac{2 \pi \text{ N}}{60}\right)^2 = \frac{m \text{ r } \pi^2 \text{ N}^2}{900}
$$

Equivalent mass of wing at location of engine: $M = \frac{33}{140} \text{ m}_w = \frac{33}{140} \text{ (a b } \ell \text{ }\rho\text{)}$
Equation of motion: $M \ddot{x} + k x = m \text{ r } \omega^2 \sin \omega t$

Maximum steady state displacement of wing at location of engine:

$$
X = \left| \frac{m r \omega^{2}}{k - M \omega^{2}} \right| = \left| \frac{\left(\frac{m r \pi^{2} N^{2}}{900} \right)}{\left\{ \frac{E b a^{3}}{4 \ell^{3}} - \frac{33}{140} a b \ell \rho \left(\frac{2 \pi N}{60} \right)^{2} \right\}} \right|
$$

$$
= \left| \frac{m r \ell^{3} N^{2}}{22.7973 E b a^{3} - 0.2357 \rho a b \ell^{4} N^{2}} \right|
$$

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2. Rao P. 3.25 Forced response of an undamped system

Equation of motion for rotation about O: Io θ = - k $\frac{\theta \ell}{4} \frac{\ell}{4}$ - k $\frac{\theta 3 \ell}{4} \frac{3 \ell}{4}$ + M₀ cos ω t
i.e., I₀ θ + $\left(\frac{5}{8}$ k $\ell^2\right)$ θ = M₀ cos ω t where $J_0 = \frac{1}{12} m \ell^2 + m \left(\frac{\ell}{4}\right)^2 = \frac{7}{48} m \ell^2 = \frac{7}{48} (10) (1^2) = 1.4583 \text{ kg} - m^2$ and $\omega = 1000$ rpm = 104.72 rad/sec. Steady state solution is:

$$
\theta_{\rm p}({\rm t}) = \Theta \, \cos \, \omega \, {\rm t}
$$

where

$$
\Theta = \frac{M_0}{\frac{5}{8} \text{ k } \ell^2 - J_0 \omega^2} = \frac{100}{5000 \left(\frac{5}{8}\right) (1^2) - 1.4583 \left(104.72^2\right)} = -0.007772 \text{ rad}
$$

Forced response of a damped system

 $M_t = M_o \cos \omega t$, $k_t = k_{t1} + k_{t2}$

Equation of motion:

 $J_0 \ddot{\theta} + C_t \dot{\theta} + (k_{t_1} + k_{t_2}) \theta = M(t) = M_0 \cos \omega t$ (1) For the given data, E_p . (1) becomes

$$
0.05 \frac{1}{\theta} + 2.5 \frac{1}{\theta} + 7000 \theta = 200 \cos 500 t \qquad (2)
$$

steady state response of the turbine rotor can be expressed, similar to Egs. (3,25), (3,28) and (3,29) for a torsional system, as

$$
\Theta_{\mu}(t) = \Theta \cos(\omega t - \phi) \tag{3}
$$

where

$$
\Theta = \frac{M_o}{\left\{ \left(k_t - J_o \omega^2 \right)^2 + C_t^2 \omega^2 \right\}^{\frac{1}{2}}}
$$
(4)

and

$$
\phi = \tan^{-1} \left(\frac{C_{\frac{1}{2}} \omega}{k_{\frac{1}{2}} - \mathbb{J}_0 \omega^2} \right) \tag{5}
$$

For the given data, $J_0 = 0.05$, $M_0 = 200$, $k_f = 7000$, $C_f = 2.5$, $\omega = 500$ Hence $Egs \cdot (4)$ and (5) give

$$
\Theta = \frac{200}{[(7000 - 0.05 \times 25 \times 10^4)]^2 + (2.5)^2 (25 \times 10^4)]^{\frac{1}{2}}}
$$

= 6.2868 x 10⁻⁶ rad

$$
\phi = \tan^{-1}\left(\frac{2.5 \times 500}{7000 - 0.05 \times 250000}\right)
$$

= $\tan^{-1}\left(-\frac{1250}{5500}\right) = \tan^{-1}\left(-0.2273\right)$
= $-12.8043^{\circ} = -0.2235 \text{ rad}$

4. Rao P. 3.45 Forced response of a damped system

$$
\frac{X}{Y} = \left[\frac{k^2 + c^2 \omega^2}{\left[k - m \omega^2\right]^2 + c^2 \omega^2} \right]^{\frac{1}{2}} .sp
$$
\nor\n
$$
\frac{10^{-6}}{Y} = \left[\frac{\left(10^6\right) + \left(10^3 \left(200 \pi\right)\right)^2}{\left[10^6 - \left(\frac{5000}{9.81}\right) \left(200 \pi\right)^2 \right]^2 + \left\{ \left(10^3\right) \left(200 \pi\right)\right\}^2 \right]^{\frac{1}{2}}}{\text{or } Y = 169.5294 \left(10^{-6}\right) m}
$$

5. Rao P. 3.47 Forced response of a damped system

m = 100 kg, $F_0 = 100$ N, $X_{max} = 0.005$ m at $\omega = 300$ rpm = 31.416 rad/sec.
Equations (3.33) and (3.34) yield:

$$
\omega = \omega_{\rm n} \sqrt{1 - 2 \zeta^2} = \sqrt{\frac{\rm k}{m}} \sqrt{1 - 2 \zeta^2} = 31.416
$$

or k (1 - 2 \zeta^2) = (100) (31.416²) = 98,696.5056
_{F₀} 1 = 0.005 (1)

and
$$
X_{\text{max}} = \delta_{\text{st}} \frac{1}{2 \varsigma \sqrt{1 - \varsigma^2}} = \frac{1}{k} \frac{1}{2 \varsigma \sqrt{1 - \varsigma^2}} = 0.005
$$

or $k \varsigma \sqrt{1 - \varsigma^2} = \frac{F_0}{2 (0.005)} = 10,000.0$ (2)

Divide Eq. (1) by (2) :

$$
\frac{1-2\zeta^2}{\zeta\sqrt{1-\zeta^2}} = 9.8696\tag{3}
$$

Squaring Eq. (3) and rearranging leads to:

$$
101.4090\,\zeta^4 - 101.4090\,\zeta^2 + 1 = 0 \quad \text{or} \quad \zeta = 0.0998, \, 0.9950
$$

Using $\zeta = 0.0998$ in Eq. (1), we obtain

$$
k = \frac{98696.5056}{1 - 2 (0.0998^2)} = 100,702.4994 N/m
$$

Since
$$
\zeta = \frac{c}{2 m \omega_n}
$$
, we find

$$
c = 2 m \omega_n \zeta = 2 (100) \sqrt{\frac{100702.4944}{1000}} (0.0998) = 633.4038 \text{ N-s/m}
$$

6. Rao P. 3.55 Response of a system under the base harmonic motion

 $\ddot{y}(t) = \ddot{x}_g(t) = A \cos \omega t$; $\dot{y}(t) = \frac{A}{\omega} \sin \omega t + B_1$ $\begin{picture}(120,140)(-20,140$ $\mathcal{H}(t) = -\frac{A}{\sqrt{2}} \cos \omega t + B_1 t + B_2$ Assuming $y(o) = \dot{y}(o) = 0$, we get $y(t) = -\frac{A}{\sqrt{a^2}} \cos \omega t$ Equation of motion: $m\ddot{x} + k(x-\ddot{x}) = 0$ *i.e.*, $m\frac{1}{2} + k\frac{1}{2} = -m\frac{3}{2} = -m\frac{2}{3}(t) = -mA\cos\omega t$ where $3 = x - 3$ Solution is: $\frac{1}{3}(t) = \frac{-mA cos \omega t}{\kappa - m \omega^2}$ \therefore $x(t) = \frac{3}{t}(t) + \frac{y(t)}{s} = -\left(\frac{\pi}{k-m\omega^2} + \frac{l}{\omega^2}\right)A$ cos ωt

7. Rao P. 3.75 Rotating unbalance Let width = 0.5 m and thickness = t m. $I = \frac{1}{12} (0.5) t^3 = \frac{t^3}{24} m^4$ $I = \frac{1}{12} (0.5) t^2 = \frac{v}{24} m^3$
 $k = \frac{3EI}{l^3} = \frac{3 (2.07 \times 10^{11}) (t^3/24)}{(5)^3} = 2.07 \times 10^8 t^3 N/m$
 $\omega_n = \sqrt{\frac{k}{M + 0.2357 m}}$ $\omega_n = \sqrt{\frac{\kappa}{M + 0.2357 \text{ m}}}$

where $m = \text{mass of beam} = (5 \times 0.5 \times t) (\frac{76.5 \times 10^3}{9.81}) = 19495.41 t$
 $\omega_n = \sqrt{\frac{2.07 \times 10^8 \text{ t}^3}{75 + 0.2357 (19495.41 t)}}$ $r = \frac{19}{\omega_n} = 125.664 \sqrt{\frac{75 + 4595.0688 \text{ t}}{2.07 \times 10^8 \text{ t}^3}}$ $X = \frac{\delta_{st}}{|\Gamma^2 - 1|} = \frac{F_0}{|\Gamma^2 - 1|}$ i.e., $0.5 = \frac{5000}{(2.07 \times 10^8 \text{ t}^3)\left\{(125.664)^2 \left[\frac{75 + 4595.0688 \text{ t}}{2.07 \times 10^8 \text{ t}^3}\right] - 1\right\}}$ i.e., 1.3108×10^{4} t³ - 4595.069 t - 74.367 = 0 By trial and error, the value of t is found as $t \approx 0.6 \text{ m}.$
Since this is too large, we can start with a new width such as

- **8.** Rao P. 3.92 Coulomb damping $m = 25 kg$, $k = 10000 N/m$, $\mu = 0.3$ $69 = 8$ Hz = 50.2656 rad/s $X = 0.2$ m E_8 . (3.88) gives $C_{eg} = \frac{4 \mu N}{\pi \omega n} = \frac{4 (0.3) (25 \times 9.81)}{\pi (50.2656) (0.2)}$ = 9.3183 $N - \frac{s}{m}$ Note: It is assumed that friction force is
	- Small compared to Fo in finding the equivalent viscous damping constant of the system.

9. Rao P. 3.97 Other types of damping

Damping force = $F = C(\dot{x})^n$ Energy dissipated per quarter cycle during harmonic motion x(t)= X sin wt $\frac{\Delta W}{4} = \int_{0}^{\frac{\pi}{2}} c(x)^n dx = \int_{0}^{\frac{\pi}{2}} c(x \cos \omega t)^n dx$ is But $dx = \dot{x} dt = \omega X \cos \omega t \cdot dt$

$$
\Delta W = 4c \omega^{n+1} X^{n+1} \int_{0}^{\pi/2} \cos^{n+1} \omega t \cdot dt
$$

\n
$$
= 4c \omega^{n+1} X^{n+1} \left\{ \frac{1}{(n+1)\omega} \cos^{n} \omega t \cdot \sin \omega t \Big|_{0}^{\pi/2} + \frac{n}{n+1} \int_{0}^{\pi/2} \cos^{n-1} \omega t \cdot dt \right\}
$$

\n
$$
= 4c \omega^{n+1} X^{n+1} \left(\frac{n}{n+1} \right) \int_{0}^{\pi/2} \cos^{n-1} \omega t \cdot dt
$$

Equating this expre

$$
c_{e_{\tilde{g}}} = \frac{4 c \omega^{n} x^{n-1}}{\pi} \left(\frac{n}{n+1}\right) \int_{0}^{\pi/2} \omega^{n-1} \omega t \, dt \equiv c \omega^{n} x^{n-1} \alpha,
$$

where $\alpha_{n} = \frac{4}{\pi} \left(\frac{n}{n+1}\right) \int_{0}^{\pi/2} \omega^{n-1} \omega t \, dt \quad --- \quad (E_{1})$

For example, for $n=2$, (E_1) becomes

$$
\alpha_n = \frac{4}{\pi} \left(\frac{2}{3} \right) \int_0^{\pi/2} \cos \omega t \, dt = \frac{8}{3\pi} \left(\frac{\sin \omega t}{\omega} \right)_0^{\pi/2} = \frac{8}{3\pi \omega}
$$

and hence $C_{\omega} = \frac{8 \cos X}{\omega}$

which can be seen to be same as the expression found in Example 3.7.

For few other values of n, xn can be found as follows: $---2---3$ -----4 ----- $\mathbf{1}$ -- n---- $\frac{8}{3\pi}$ 32 $\frac{3}{409}$ α_n $15 \pi 49$

The amplitude can be found as

$$
X = \frac{F_0}{\sqrt{(k - m\omega^2)^2 + c_{eg}^2 \omega^2}} = \frac{F_0}{\sqrt{\kappa^2 (1 - r^2)^2 + c_{eg}^2 \omega^2}}
$$

$$
= \frac{F_0}{\sqrt{\kappa^2 (1 - r^2)^2 + c^2 \omega^2 (n + 1) \chi^2 (n - 1) \omega_n^2}}
$$